

## **Some Useful Results from Calculus**

## Derivation of Gauss' Theorem

Let  $f(x, y, z)$  be a differentiable scalar function of  $(x, y, z)$ .

$$\vec{f}_1 \equiv \hat{i}f$$

By the divergence theorem,

$$\int_V \nabla \cdot \vec{f}_1 dv = \int_S \vec{f}_1 \cdot \vec{n} ds = \int_S n_x f ds$$

$$\nabla \cdot \vec{f}_1 = \frac{\partial f}{\partial x}$$

$$\int_V \hat{i} \nabla \cdot \vec{f}_1 dv = \int_V \hat{i} \frac{\partial f}{\partial x} dv = \int_S \hat{i} n_x f ds$$

Similarly,

$$\int_V \hat{j} \nabla \cdot \vec{f}_2 dv = \int_V \hat{j} \frac{\partial f}{\partial y} dv = \int_S \hat{j} n_y f ds$$

$$\int_V \hat{k} \nabla \cdot \vec{f}_3 dv = \int_V \hat{k} \frac{\partial f}{\partial z} dv = \int_S \hat{k} n_z f ds$$

Now, add the last three equations together,

$$\int_V \nabla f dv = \int_S \vec{n} f ds$$

**Example of Use of Gauss Theorem:  
Froude Krylov Surge Force on a Ship**



$$P = \rho g A e^{-kz} \cos(kx - \omega t) \quad \vec{F} = \int \int_S -p \vec{n} dS$$

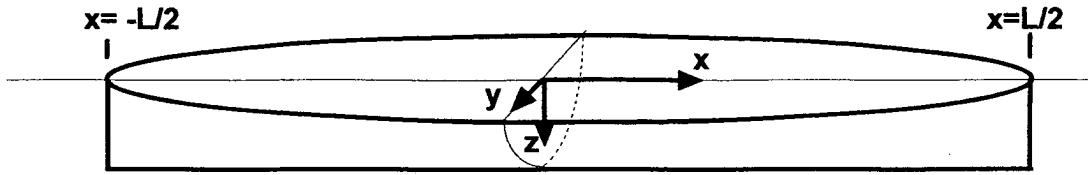
$$F_x = \hat{i} \cdot \int \int_S -P \vec{n} ds = -\hat{i} \int \int \int_V \nabla P dV$$

$$F_x = - \int \int \int_V \frac{\partial P}{\partial x} dV = \rho g A k \int \int \int_V e^{-kz} \sin(kx - \omega t) dV$$

$$\begin{aligned} F_x &\simeq \rho g A k \int \int \int_V (1 - kz) \sin(kx - \omega t) dV \\ &= \rho g A k \int_L \left[ \int \int_{\text{section}} dy dz \right] \sin(kx - \omega t) dx \\ &\quad - \rho g A k^2 \int_L \left[ \int \int_{\text{section}} z dy dz \right] \sin(kx - \omega t) dx \end{aligned}$$

$$F_x = \rho g A k \int_L S(x) \sin(kx - \omega t) dx - \rho g A k^2 \int_L z_{ca} S(x) \sin(kx - \omega t) dx$$

Example with Given Ship Shape



$$y = \frac{2W}{L^2 D^2} \left( \frac{L}{2} - x \right)^2 (D - z)^2$$

For this shape:

$$S(x) = \frac{2WD}{3L^2} \left( \frac{L}{2} - x \right)^2 \quad z_{ca} = \frac{D}{4}$$

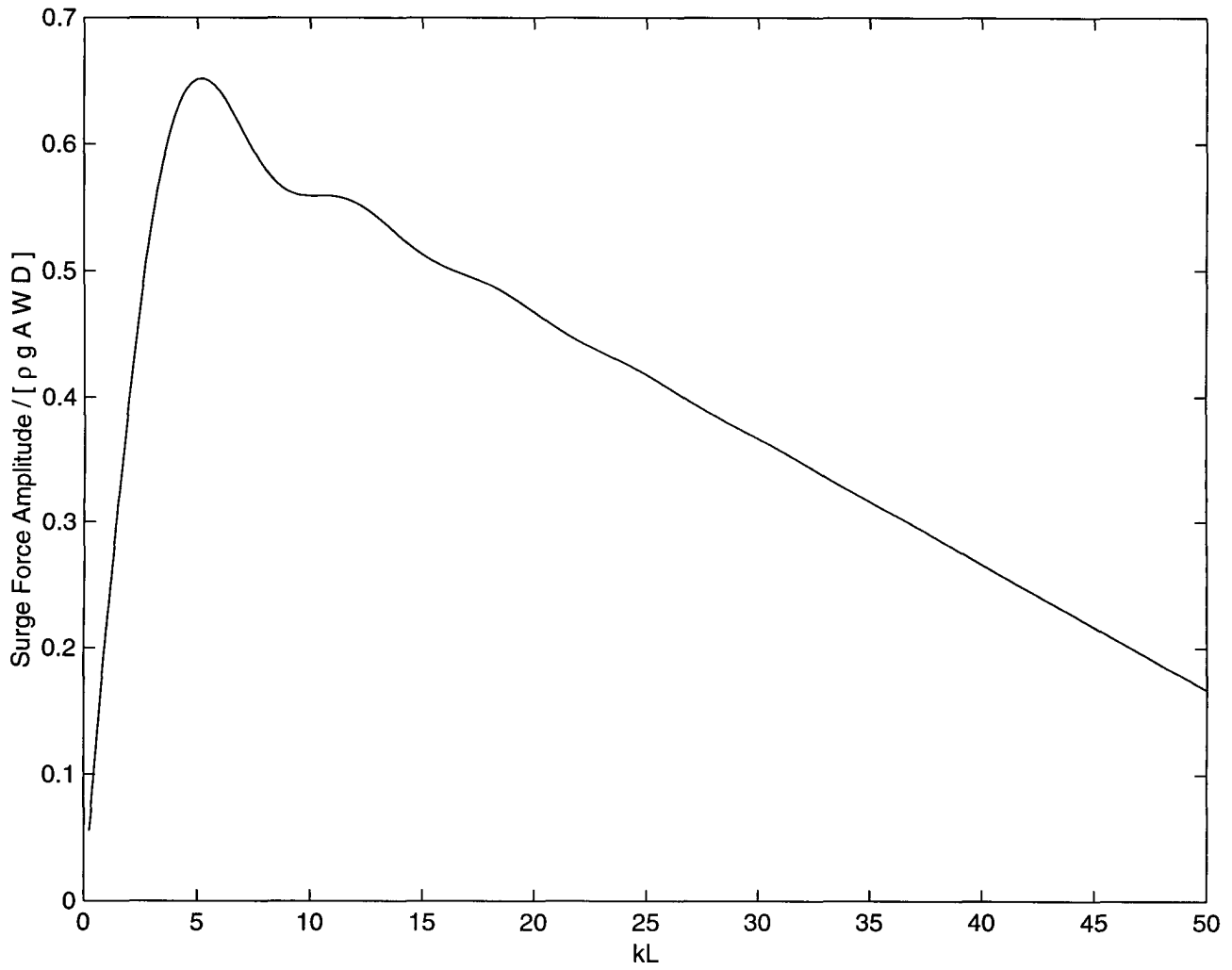
Using these values:

$$F_x = \frac{2}{3} \rho g A k \frac{WD}{L^2} \left( 1 - \frac{kD}{4} \right) \left\{ \cos \omega t \left[ -\frac{2L}{k^2} \sin \frac{kL}{2} + \frac{L^2}{k} \cos \frac{kL}{2} \right] - \sin \omega t \left[ \left( \frac{L^2}{k} - \frac{4}{k^3} \right) \sin \frac{kL}{2} + \frac{2L}{k^2} \cos \frac{kL}{2} \right] \right\}$$

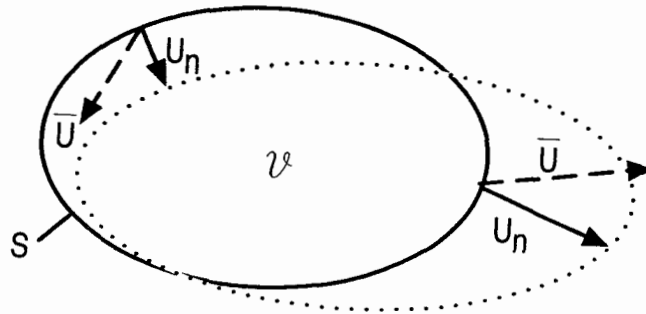
$$\frac{F_x}{\rho g A W D} = \frac{2}{3} k L \left( 1 - \frac{kL D}{4 L} \right) \left\{ \cos \omega t \left[ -\frac{2}{(kL)^2} \sin \frac{kL}{2} + \frac{1}{kL} \cos \frac{kL}{2} \right] - \sin \omega t \left[ \left( \frac{1}{kL} - \frac{4}{(kL)^3} \right) \sin \frac{kL}{2} + \frac{2}{(kL)^2} \cos \frac{kL}{2} \right] \right\}$$

$$\left[ \frac{F_x}{\rho g A W D} \right]_{\max} = \frac{2}{3} k L \left( 1 - \frac{kL D}{4 L} \right) \left\{ \left[ -\frac{2}{(kL)^2} \sin \frac{kL}{2} + \frac{1}{kL} \cos \frac{kL}{2} \right]^2 + \left[ \left( \frac{1}{kL} - \frac{4}{(kL)^3} \right) \sin \frac{kL}{2} + \frac{2}{(kL)^2} \cos \frac{kL}{2} \right]^2 \right\}^{1/2}$$

```
% m-file script for gaussexp
tt = 2.0/3.0;
DoL = 0.06;
DoLf = DoL/4.;
m = 1:1:200;
kL = 0.25.*m;
kLi = 1.0 ./ kL;
sn = sin(kL ./ 2.0);
cs = cos(kL ./ 2.0);
fnd = tt .* kL .* (1.0 - kL .* DoLf) .* ((( -2 ./ (kL.^ 2)) .* sn + kLi .* ✓
cs) .^ 2 ...
+ ( ( kLi -4.0 .* (kLi .^3)) .* sn + (2.0 ./ (kL.^2)).* cs) .^2) .^ 0.5;
q = [kL;fnd];
fid = fopen('surge.dat','w');
fprintf(fid,'%8.3f, %9.4f\n',q);
fclose(fid);
plot(kL,fnd)
xlabel('kL')
ylabel('Surge Force Amplitude / [ \rho g A W D ]')
```



## The Transport Theorem



Let  $f(\mathbf{x}, t)$  be a differentiable scalar function of  $\mathbf{x}$  and  $t$ .

Consider the integral,

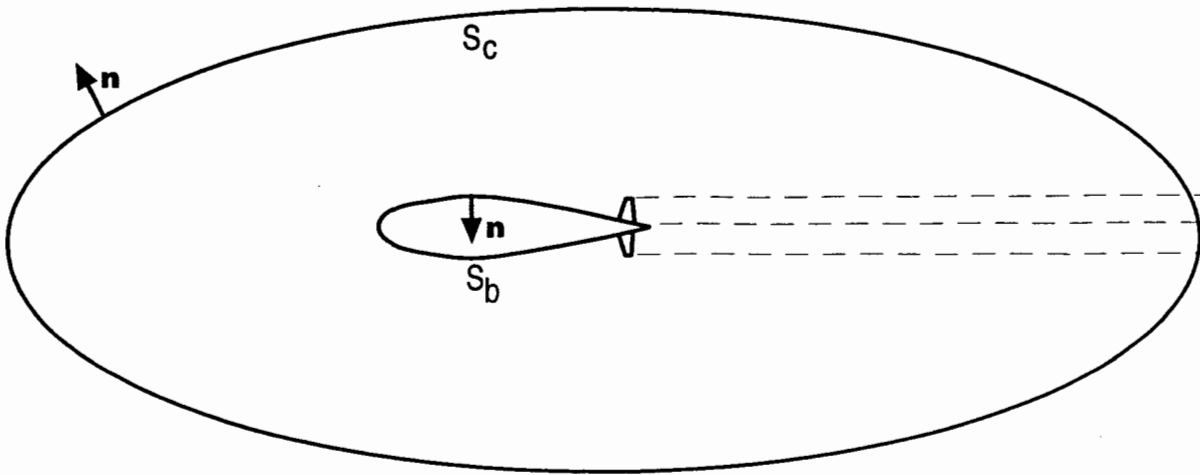
$$I(t) = \iiint_{\mathcal{V}(t)} f(\mathbf{x}, t) d\mathcal{V}$$

$f$  is changing with time and  $\mathcal{V}$  is changing with time. The normal component of the velocity of any point on the surface,  $S$  of  $\mathcal{V}$  is called  $U_n$ .

$$\frac{dI}{dt} = \iiint_{\mathcal{V}} \frac{\partial f}{\partial t} d\mathcal{V} + \iint_S f U_n dS = \iiint_{\mathcal{V}} \left\{ \frac{\partial f}{\partial t} + \nabla \cdot (f \vec{U}) \right\} d\mathcal{V}$$

Note that if  $\vec{U}$  is the fluid velocity, the surface  $S$  is a material surface and the Transport Theorem is simply the integral form of the Substantial Derivative.

## Pressure Forces and Moments on an Object



$$\mathbf{F} = \int \int_{S_b} p \mathbf{n} dS \quad \mathbf{M} = \int \int_{S_b} p (\mathbf{r} \times \mathbf{n}) dS$$

Now use the (unsteady) Bernoulli equation:

$$\mathbf{F} = -\rho \int \int_{S_b} \left[ \frac{\partial \phi}{\partial t} + \frac{1}{2} \nabla \phi \cdot \nabla \phi \right] \mathbf{n} dS$$

$$\mathbf{M} = -\rho \int \int_{S_b} \left[ \frac{\partial \phi}{\partial t} + \frac{1}{2} \nabla \phi \cdot \nabla \phi \right] (\mathbf{r} \times \mathbf{n}) dS$$

The following results from applying Gauss, Transport and divergence theorems and boundary conditions:

$$\mathbf{F} = -\rho \frac{d}{dt} \int \int_{S_b} \phi \mathbf{n} dS - \rho \int \int_{S_c} \left[ \frac{\partial \phi}{\partial n} \nabla \phi - \mathbf{n} \frac{1}{2} \nabla \phi \cdot \nabla \phi \right] dS$$

$$\mathbf{M} = -\rho \frac{d}{dt} \int \int_{S_b} \phi (\mathbf{r} \times \mathbf{n}) dS - \rho \int \int_{S_c} \mathbf{r} \times \left[ \frac{\partial \phi}{\partial n} \nabla \phi - \mathbf{n} \frac{1}{2} \nabla \phi \cdot \nabla \phi \right] dS$$