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6.013/ESD.013J Electromagnetics and Applications, Fall 2005

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I. Ohm's Law in Moving Media

Force on moving charge: $\vec{f} = q(\vec{E} + \vec{v} \times \vec{B})$

Consider force on moving charge in reference frame (denoted as prime (') frame) moving at charge velocity \vec{v} . Then $\vec{f}' = q\vec{E}'$ as in the moving frame the relative velocity is zero.

With \vec{v} constant, \vec{f} and \vec{f}' are inertial frames (non-accelerating) so that:

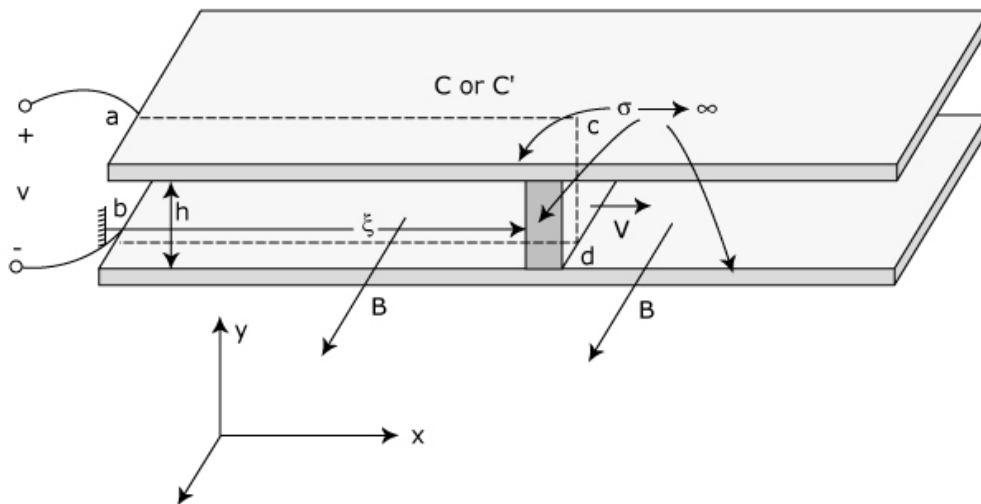
$$\vec{f} = \vec{f}' \Rightarrow q\vec{E}' = q(\vec{E} + \vec{v} \times \vec{B}) \Rightarrow \vec{E}' = \vec{E} + \vec{v} \times \vec{B}$$

in primed frame: $\vec{J}' = \sigma\vec{E}' = \sigma(\vec{E} + \vec{v} \times \vec{B})$

If system is charge neutral, as is usual case in MQS systems

$$\vec{J} = \vec{J}' = \sigma(\vec{E} + \vec{v} \times \vec{B})$$

II. Moving Media MQS Problem



A pair of parallel perfectly conducting plates are short-circuited by a moving perfectly conducting bar. Because of the magnetic field B , a voltage v is induced which can be computed either by integrating the induction equation around the fixed loop C' that passes through the bar or by integrating the induction equation around a loop C that expands in area as the bar moves to the right. The field transformation of (6.1.38) guarantees that both integrations will give the same result.

Moving Contour C

$$\oint_C \bar{E}' \cdot d\bar{l} = -\frac{d}{dt} \int_S \bar{B} \cdot \bar{n} da$$

$$-v = -\frac{d}{dt} [-Bh\xi]$$

\bar{B} and \bar{n} in opposite directions

$$v = -Bh \frac{d\xi}{dt} = -BhV$$

Stationary Contour C'

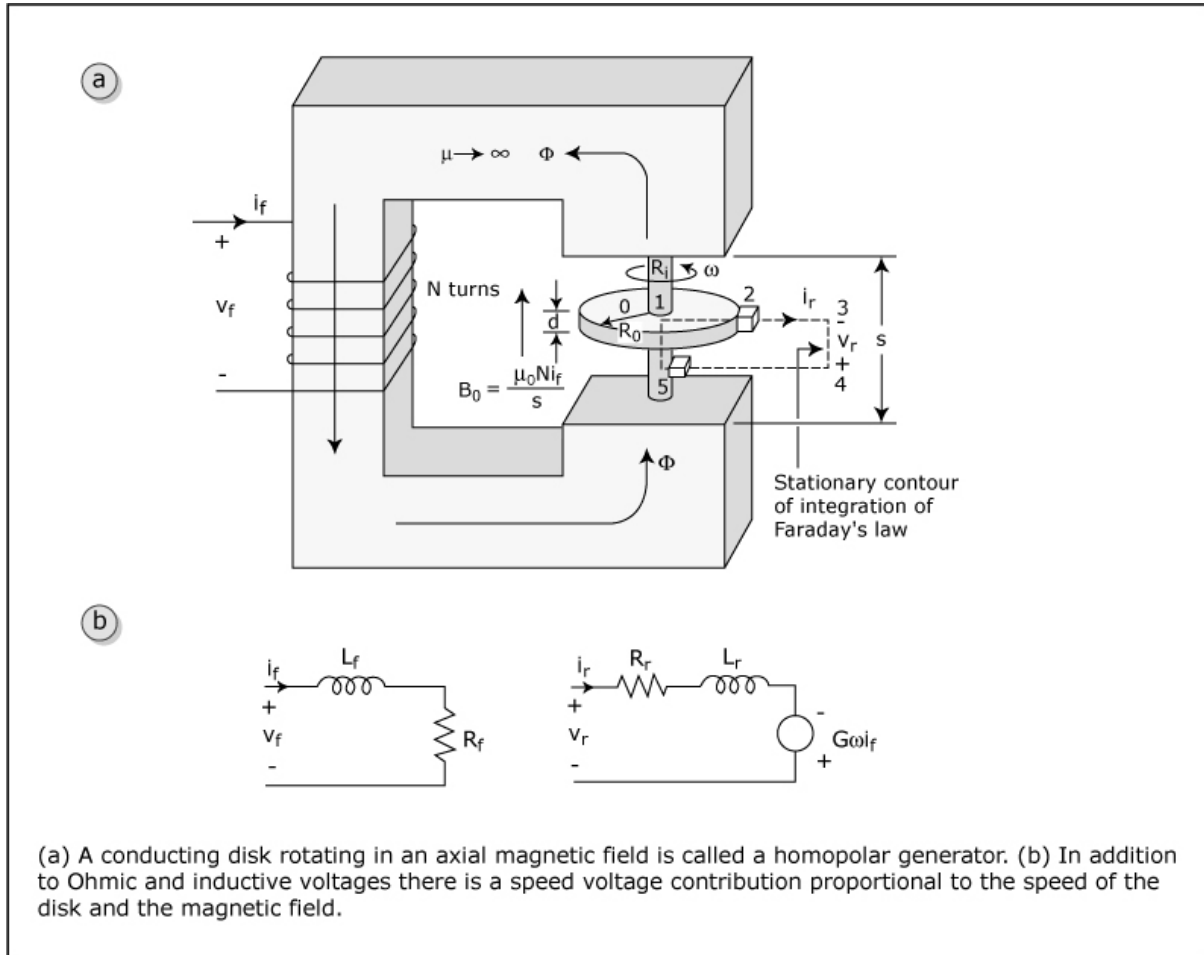
$$\oint_{C'} \bar{E} \cdot d\bar{l} = -\frac{d}{dt} \int_{S'} \bar{B} \cdot \bar{n} da = 0$$

$\bar{E}' = 0 = \bar{E} + \bar{v} \times \bar{B}$ in moving perfect conductor

$$-v + (\bar{v} \times \bar{B})_y = 0$$

$$v = -BhV$$

III. Faraday's Disk (Homopolar Generator)



$$B_0 = \frac{\mu_0 N i_f}{s}$$

$$\vec{J} = \sigma(\vec{E} + \vec{v} \times \vec{B}) \Rightarrow \vec{E} = \frac{\vec{J}}{\sigma} - \vec{v} \times \vec{B} \Rightarrow E_r = \frac{i_r}{2\pi\sigma dr} - \omega r B_0$$

$$\oint_L \vec{E} \cdot d\vec{l} = \int_1^2 E_r dr + \underbrace{\int_3^4 \vec{E} \cdot d\vec{l}}_{-v_r} = 0$$

$$v_r = \int_1^2 E_r dr = \int_{R_1}^{R_0} \left(\frac{i_r}{2\pi\sigma dr} - \omega r B_0 \right) dr = \frac{i_r}{2\pi\sigma d} \ln \frac{R_0}{R_1} - \frac{\omega B_0}{2} (R_0^2 - R_1^2)$$

$$= i_r R_r - G \omega i_f$$

$$R_r = \frac{\ln \frac{R_o}{R_i}}{2\pi\sigma d}, \quad G = \frac{\mu_0 N}{2S} (R_o^2 - R_i^2)$$

Representative Numbers: copper ($\sigma \approx 6 \times 10^7$ siemen / m), $d = 1$ mm

$$\omega = 3600 \text{ rpm} = 120 \pi \text{ rad / s}$$

$$R_o = 10 \text{ cm}, R_i = 1 \text{ cm}, B_o = 1 \text{ tesla}$$

$$v_{oc} = \frac{-\omega B_o}{2} (R_o^2 - R_i^2) \approx -1.9 \text{ V}$$

$$i_{sc} = \frac{v_{oc} 2\pi\sigma d}{\ln \left(\frac{R_o}{R_i} \right)} \approx 3 \times 10^5 \text{ amp}$$

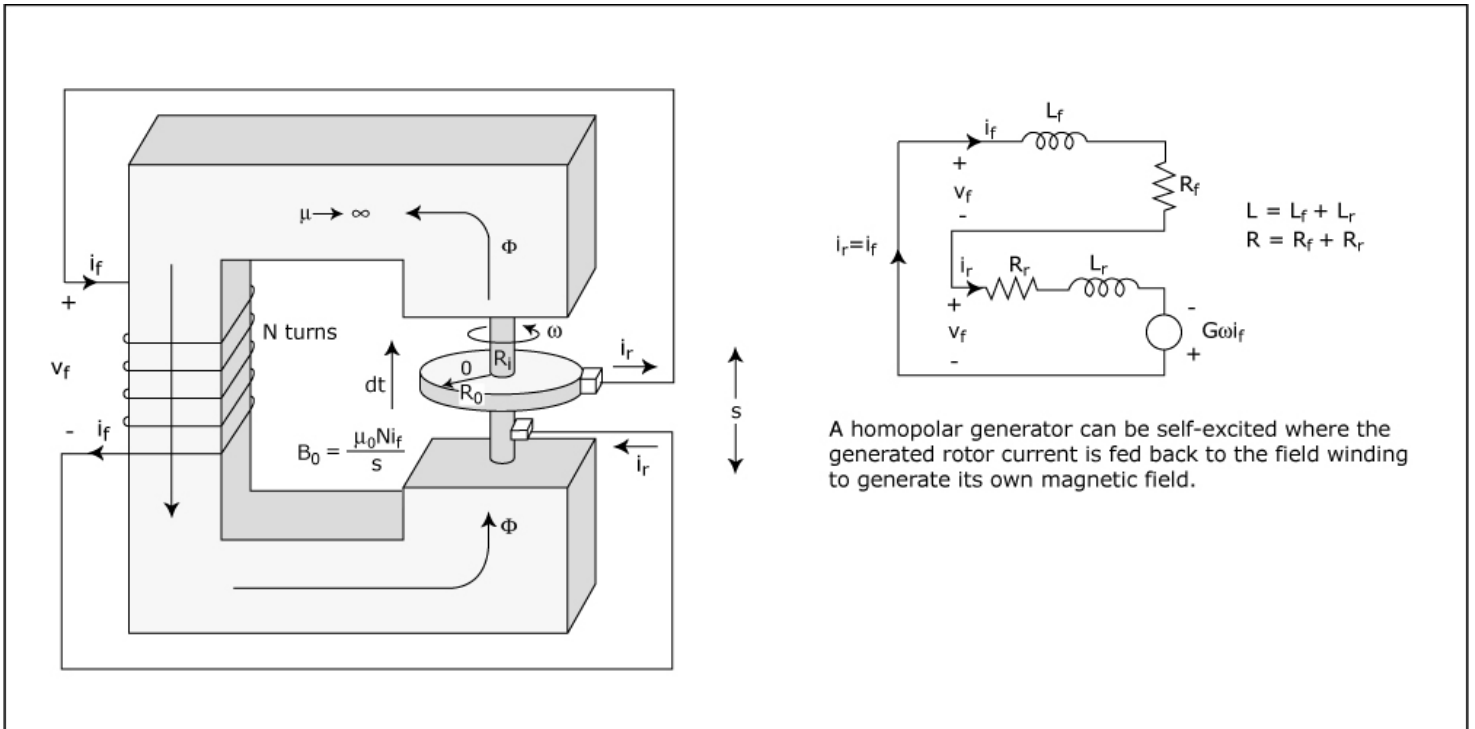
$$\bar{T} = \int_{\phi=0}^{2\pi} \int_{z=0}^d \int_{r=R_i}^{R_o} r \bar{i}_r \times (\bar{J} \times \bar{B}) r \, dr \, d\phi \, dz$$

$$= -i_r B_o \bar{i}_z \int_{R_i}^{R_o} r \, dr$$

$$= \frac{-i_r B_o}{2} (R_o^2 - R_i^2) \bar{i}_z$$

$$= -G i_f i_r \bar{i}_z$$

IV. Self-Excited DC Homopolar Generator



$$i_f = i_r \equiv i$$

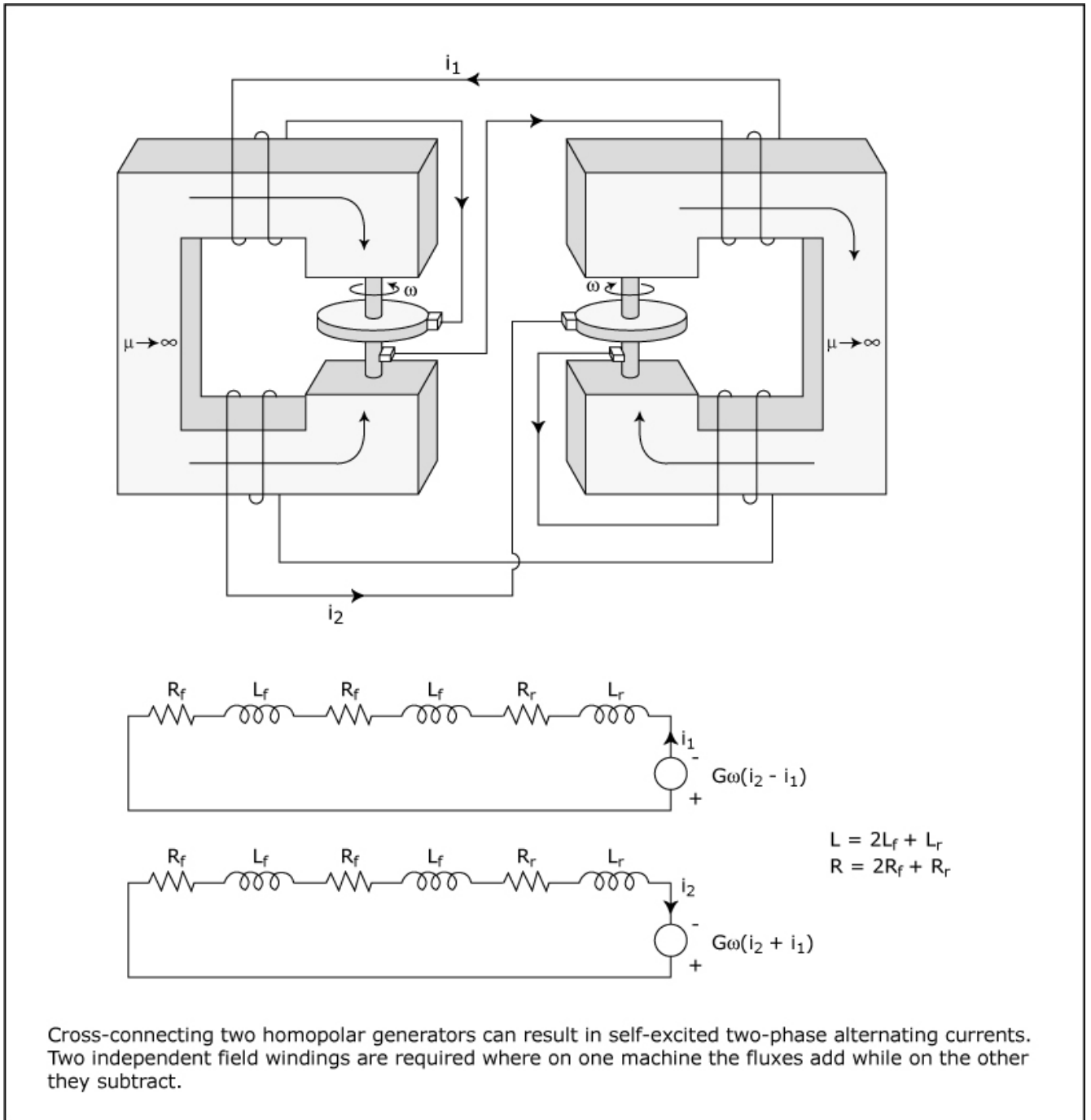
$$L \frac{di}{dt} + i(R - G\omega) = 0 ; \quad R = R_f + R_r$$

$$L = L_r + L_f$$

$$i(t) = I_0 e^{-[R-G\omega]t/L}$$

$$G\omega > R \quad \text{Self-Excited}$$

V. Self-Excited AC Homopolar Generator



$$L \frac{di_1}{dt} + (R - G\omega)i_1 + G\omega i_2 = 0$$

$$L \frac{di_2}{dt} + (R - G\omega)i_2 - G\omega i_1 = 0$$

$$i_1 = I_1 e^{st}, \quad i_2 = I_2 e^{st}$$

$$(Ls + R - G\omega)I_1 + G\omega I_2 = 0$$

$$-G\omega I_1 + (Ls + R - G\omega)I_2 = 0$$

$$(Ls + R - G\omega)^2 + (G\omega)^2 = 0$$

$$Ls + R - G\omega = \pm jG\omega$$

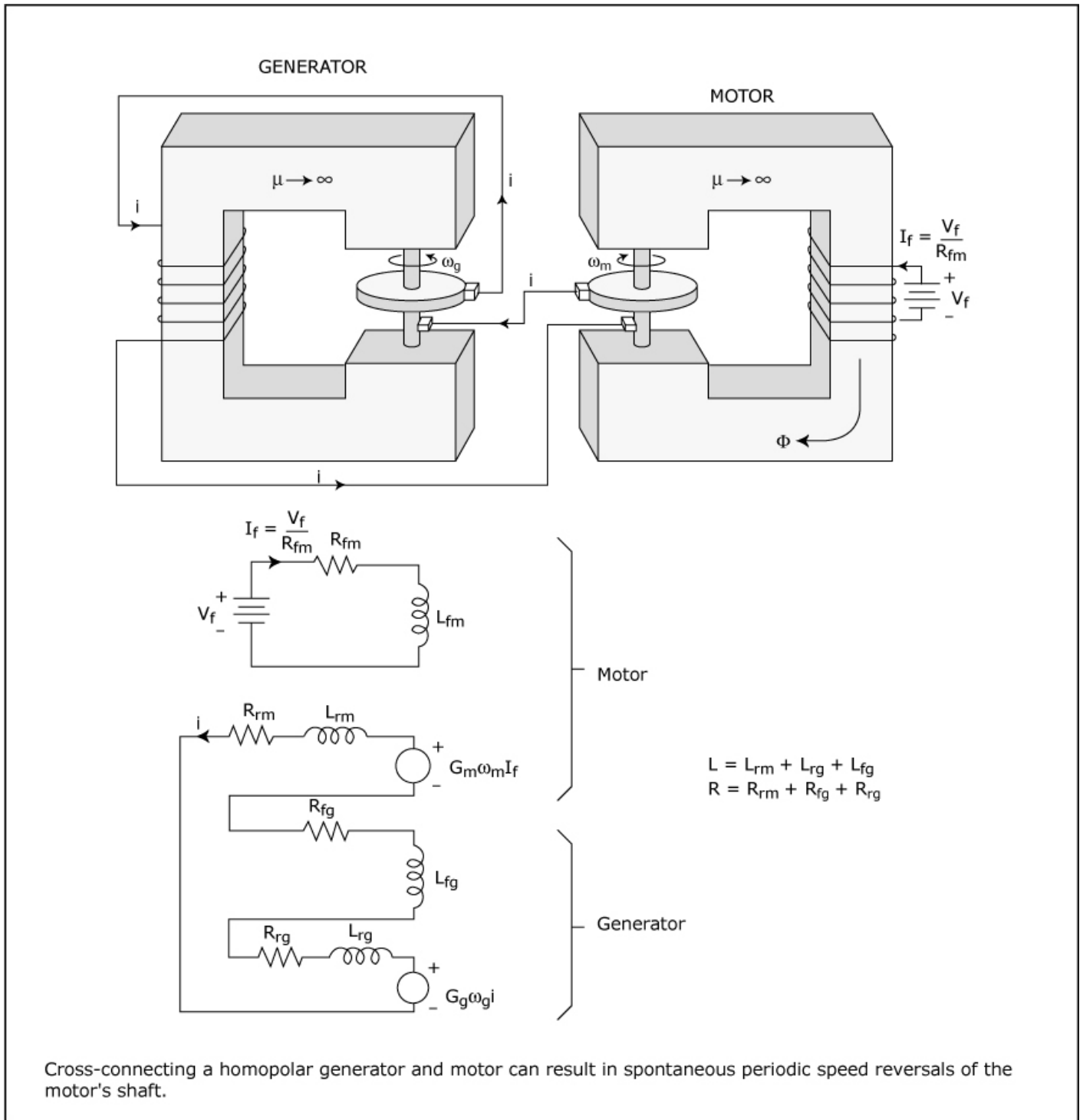
$$s = -\frac{(R - G\omega)}{L} \pm j\frac{G\omega}{L}$$

$$\frac{I_1}{I_2} = \frac{-G\omega}{(Ls + R - G\omega)} = \pm j$$

Self Excited: $G\omega > R$

Oscillation frequency: $\omega_0 = I_m(s) = G\omega/L$

VI. Self-Excited Periodic Motor Speed Reversals



$$\frac{di}{dt} + \frac{(R - G_g \omega_g)i}{L} = \frac{G_m \omega_m I_f}{L}$$

$$J \frac{d\omega_m}{dt} = -G_m I_f i$$

$$i = I e^{st}, \omega_m = W e^{st}$$

$$I \left[s + \frac{R - G_g \omega_g}{L} \right] - W \left(\frac{G_m I_f}{L} \right) = 0$$

$$I \left(\frac{G_m I_f}{J} \right) + Ws = 0$$

$$s \left[s + \frac{R - G_g \omega_g}{L} \right] + \frac{(G_m I_f)^2}{JL} = 0$$

$$s = -\frac{(R - G_g \omega_g)}{2L} \pm \left[\left(\frac{R - G_g \omega_g}{2L} \right)^2 - \frac{(G_m I_f)^2}{JL} \right]^{1/2}$$

Self-excitation: $G_g \omega_g > R$

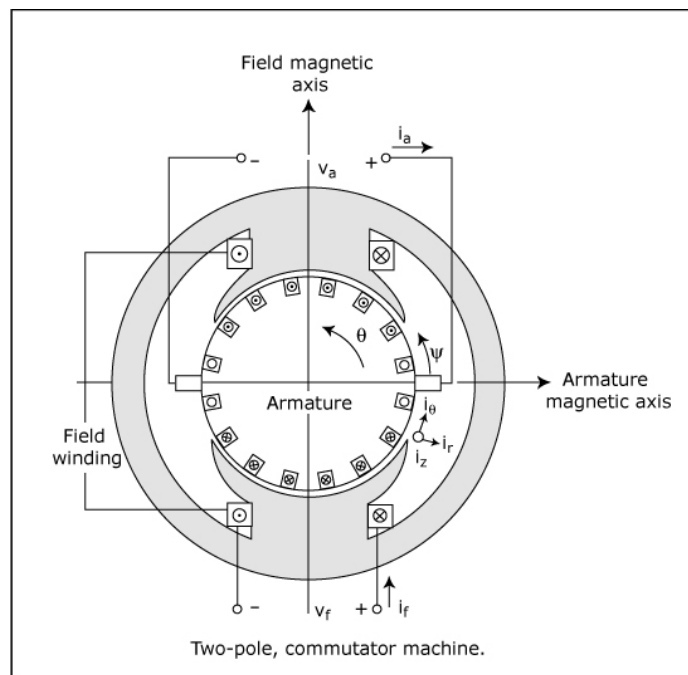
Oscillations if s has an imaginary part:

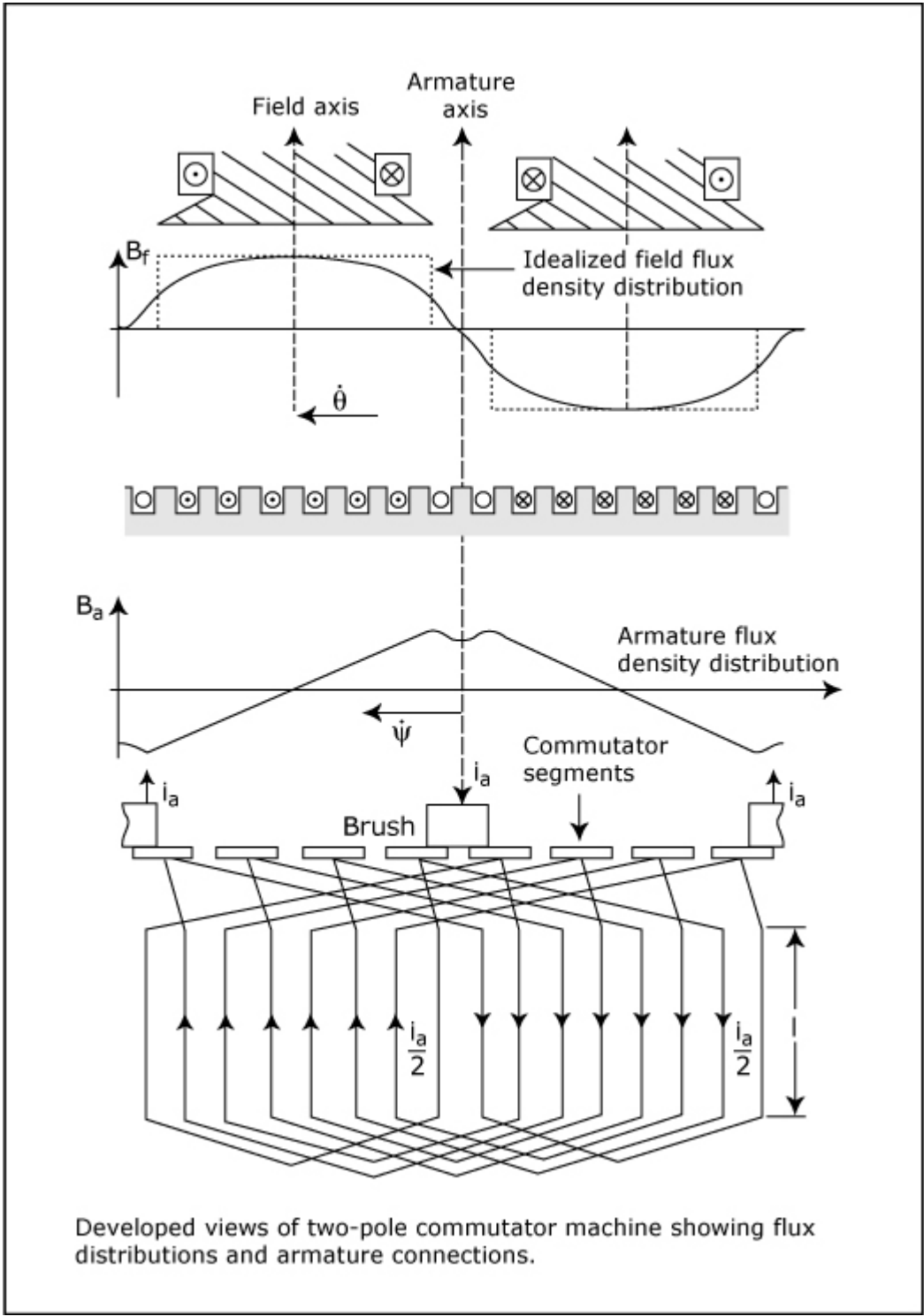
$$\frac{(G_m I_f)^2}{JL} > \left(\frac{R - G_g \omega_g}{2L} \right)^2$$

VII. DC Commutator Machines

Quasi-One Dimensional Description

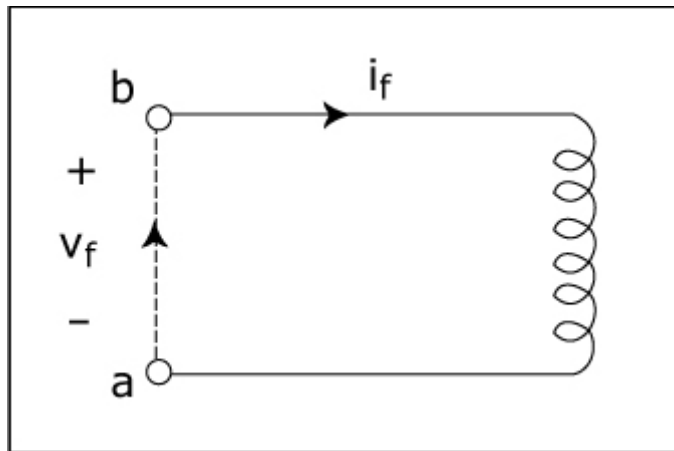
A. Electrical Equations





$$\oint_c \bar{E} \cdot d\bar{l} = -\frac{d}{dt} \int_s \bar{B} \cdot \bar{n} da$$

1. Field Winding



$$\oint_C \vec{E} \cdot d\vec{l} = -v_f + \underbrace{\int_{\text{winding}} \frac{i_f}{A\sigma} dl}_{\frac{J}{\sigma}} = -v_f + i_f R_f$$

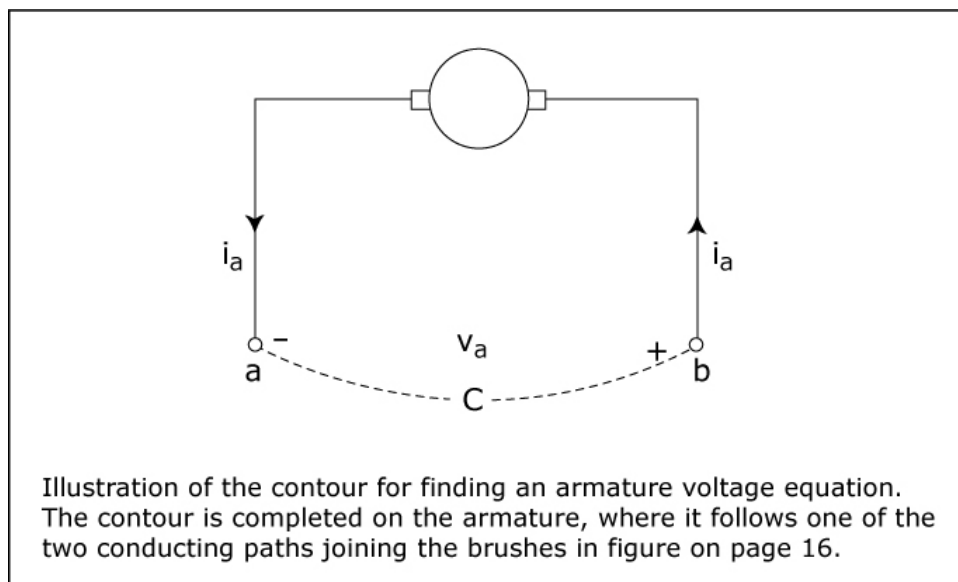
Resistance of field winding

$$\lambda_f = \int_S \vec{B} \cdot \vec{n} da = L_f i_f$$

$$-v_f + i_f R_f = -L_f \frac{di_f}{dt}$$

$$v_f = L_f \frac{di_f}{dt} + i_f R_f$$

2. Armature Winding



Reminder: $\vec{f} = q(\vec{E} + \vec{v} \times \vec{B}) = q\vec{E}'$

$$\vec{E}' = \vec{E} + \vec{v} \times \vec{B}$$

Take Stationary Contour through armature winding

$$\vec{E} = \vec{E}' - \vec{v} \times \vec{B}$$

$$\oint_C \vec{E} \cdot d\vec{l} = -v_a + \int (\vec{E}' - \vec{v} \times \vec{B}) \cdot d\vec{l}$$

$$= -v_a + \int_a^b \left(\frac{i_a}{A\sigma} + \omega R B_r \bar{i}_z \right) \cdot d\vec{l} ; \quad v = \omega R \bar{i}_\theta$$

$$\vec{B} = i_f B_r(\chi)$$

$$= -v_a + i_a R_a + \omega R (B_{rf})_{av} l N$$

$$= -\frac{d}{dt} \int_S \vec{B} \cdot d\vec{a} = -L_a \frac{di_a}{dt}$$

$$v_a = i_a R_a + L_a \frac{di_a}{dt} + G \omega i_f \quad (G i_f = l N R (B_{rf})_{av})$$

B. Mechanical Equations

$$\vec{F} = \bar{i}_\theta J_z B_r = \bar{i}_\theta \frac{i_a}{A_w} B_r, \quad \vec{f} = \vec{F} A_w l = \bar{i}_\theta i_a l B_r$$

$$T = f R = i_a l B_r R N = G i_f i_a$$

$$J \frac{d^2\theta}{dt^2} = T = G i_f i_a$$

C. Linear Amplifier

1) Open Circuit

$$v_f = V_f, \quad i_a = 0 \Rightarrow i_f = V_f / R_f$$

$$v_a = G \omega V_f / R_f$$

2) Resistively Loaded Armature (DC Generator)

$$v_a = -i_a R_L = i_a R_a + G \omega V_f / R_f$$

$$i_a = \frac{-G \omega V_f}{R_f (R_a + R_L)}$$

$$v_a = \frac{G \omega V_f R_L}{R_f (R_a + R_L)}$$

D. DC Motors

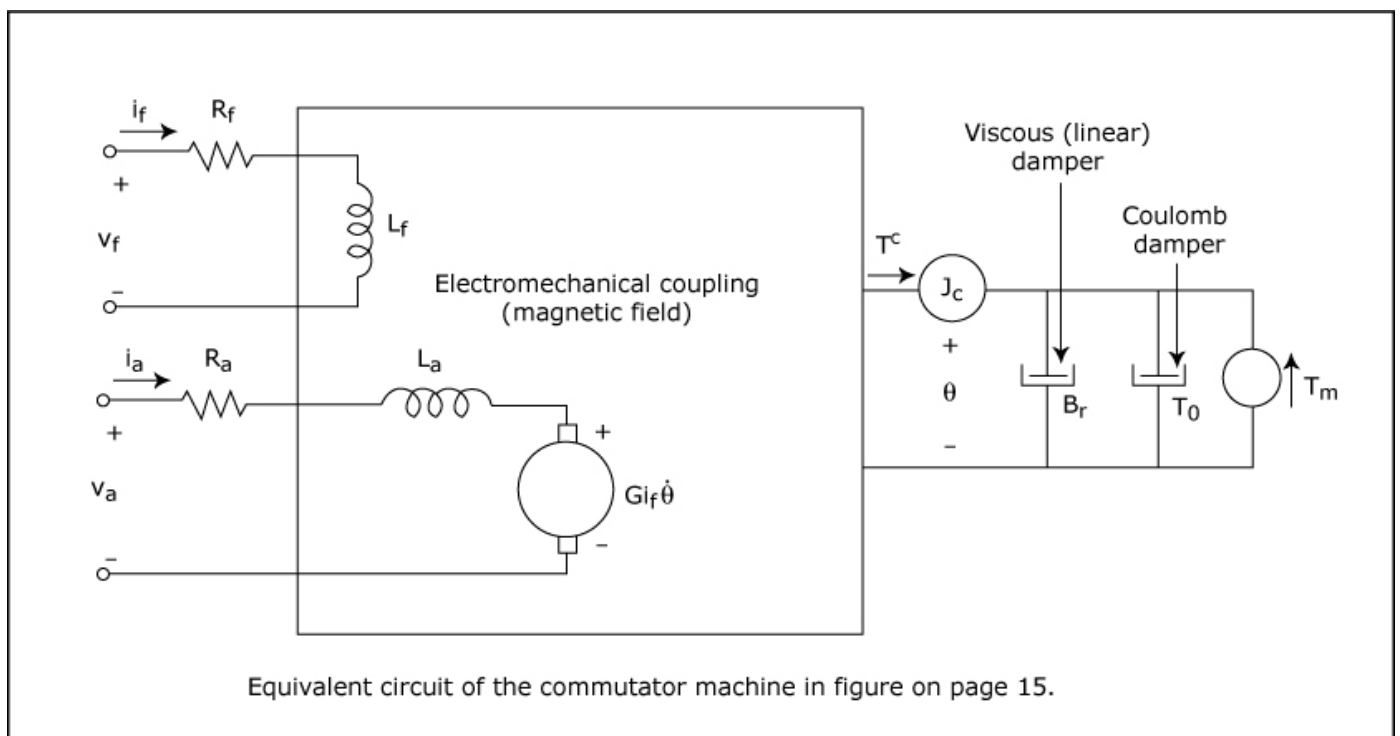
1) Shunt Excitation: $v_a = v_f = v_t$

$$v_t = i_f R_f = i_a R_a + G \omega i_f$$

$$i_f (R_f - G \omega) = i_a R_a$$

$$i_f = \frac{V_t}{R_f}, \quad i_a = \frac{V_t (R_f - G \omega)}{R_a}$$

$$T = G i_f i_a = G \left(\frac{V_t}{R_f} \right)^2 \frac{(R_f - G \omega)}{R_a}$$



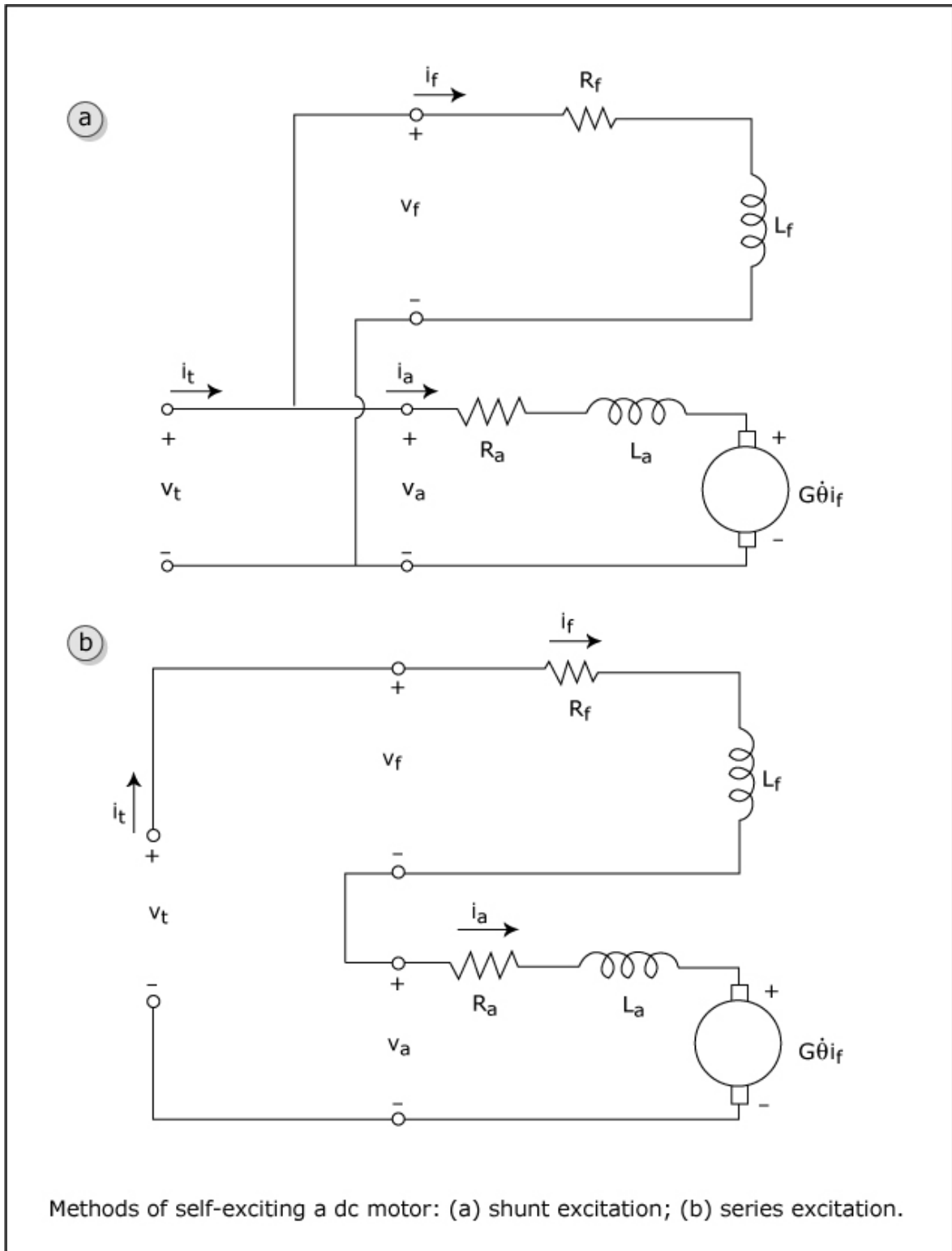
2) Series: $i_a = i_f = i_t$

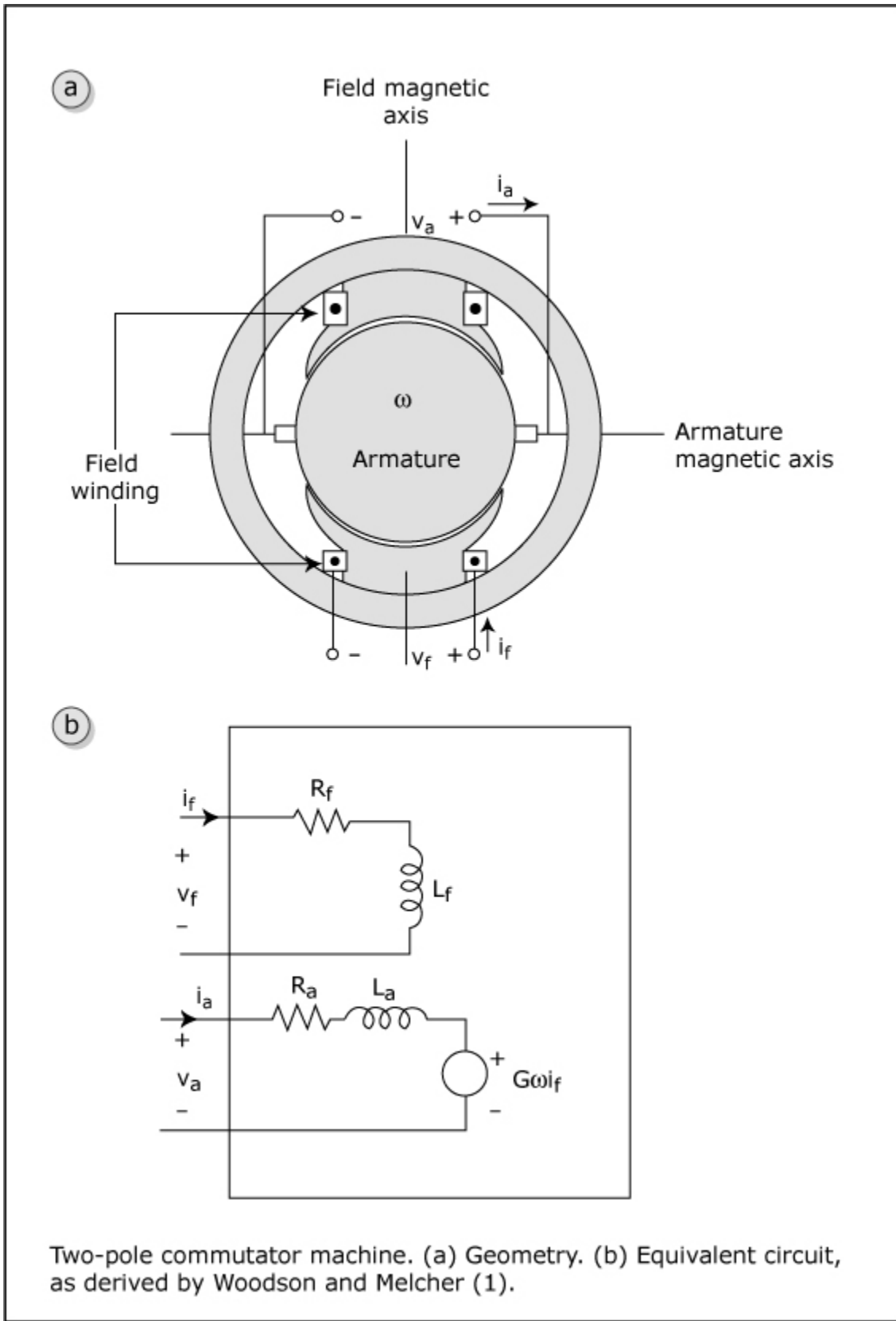
$$i_t (R_f + R_a + G\omega) = v_t$$

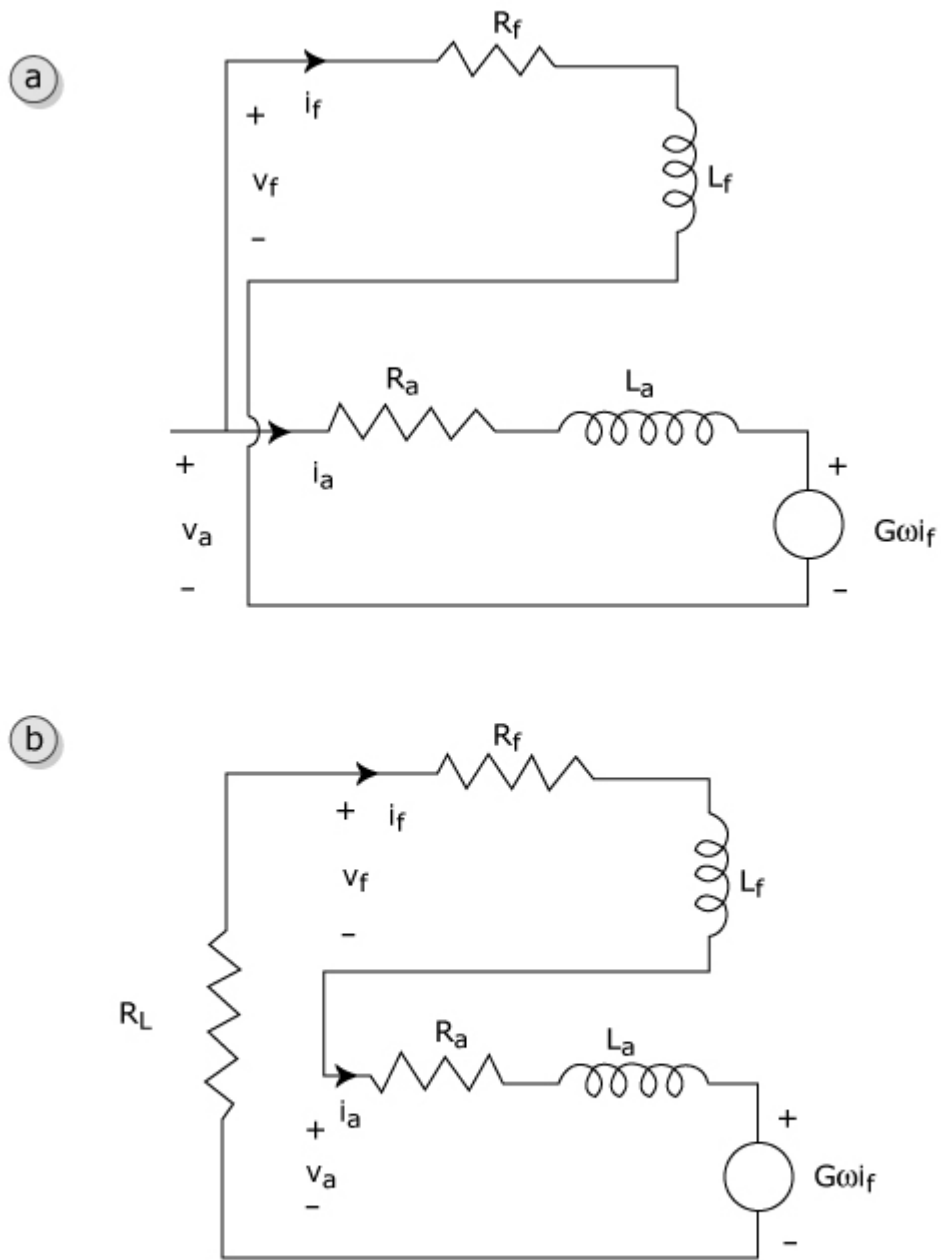
$$i_t = \frac{v_t}{(R_f + R_a + G\omega)}$$

$$T = G i_t^2 = G \frac{v_t^2}{(R_f + R_a + G\omega)^2}$$

VIII. Self-Excited Machines

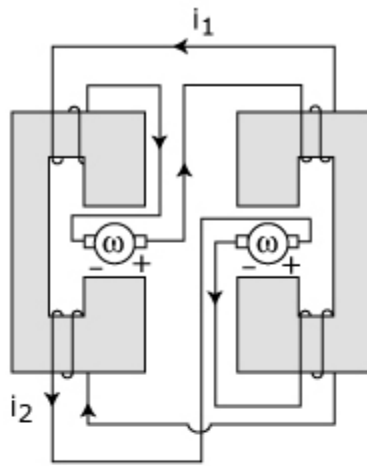




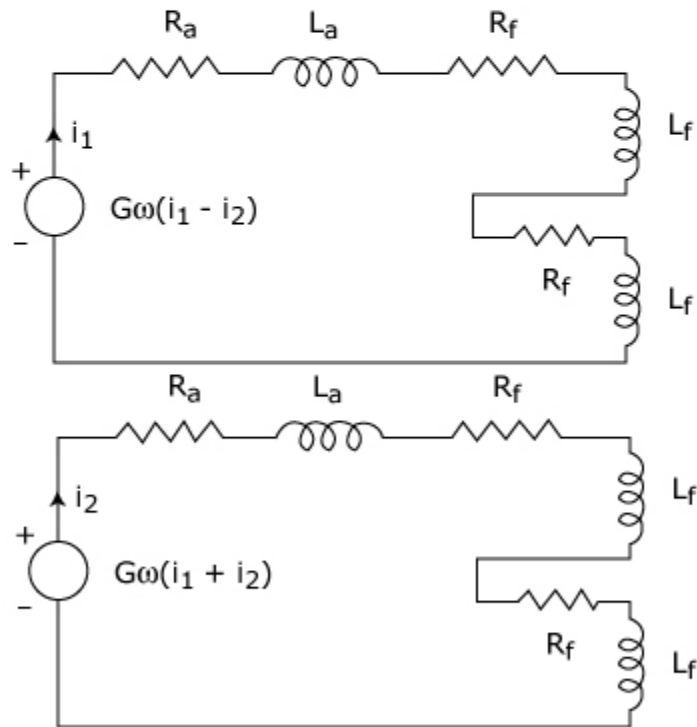


Equivalent circuit models for shunt and series self-excited generators.
 (a) Open-circuit shunt. (b) Series with load resistor.

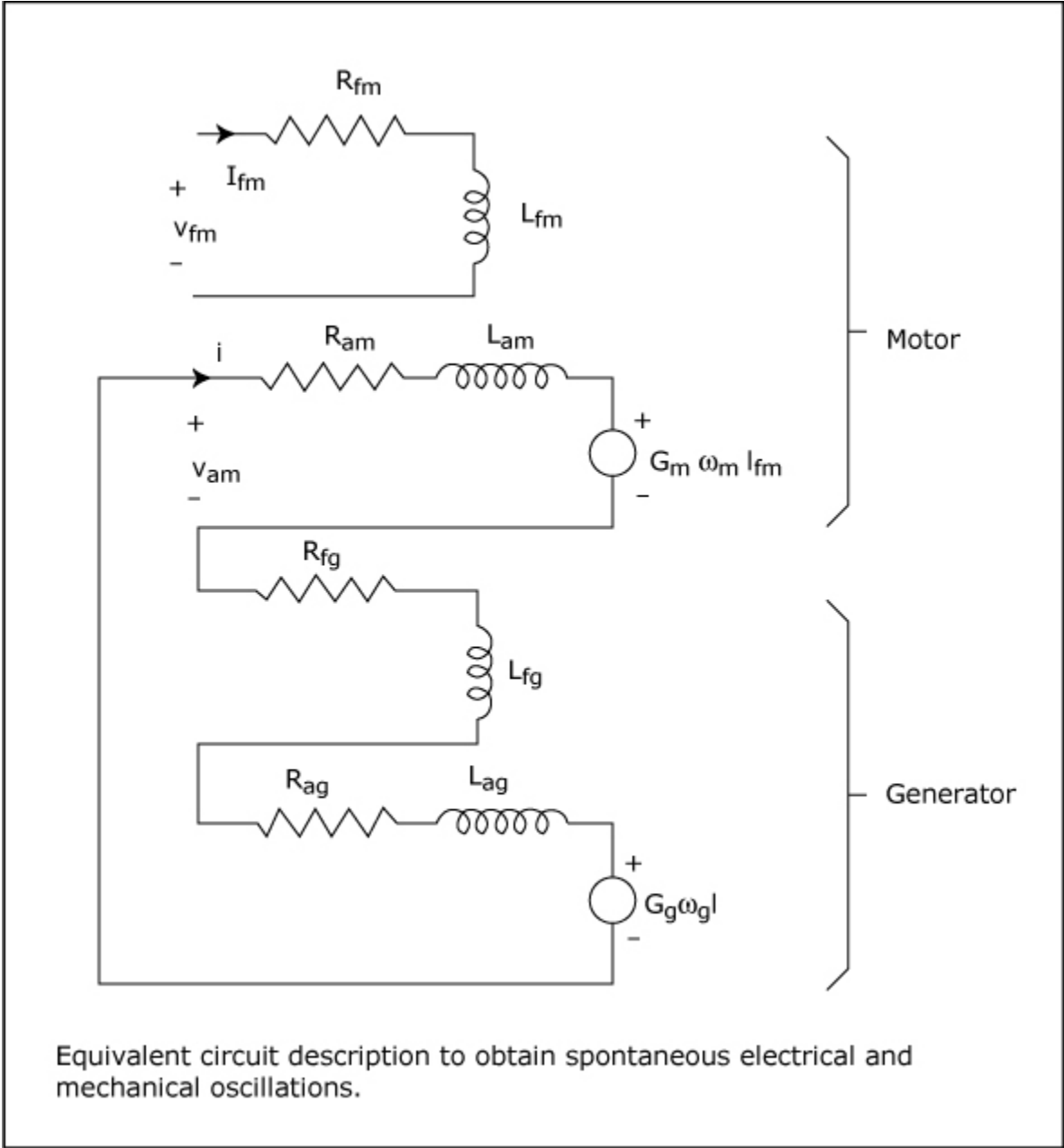
(a)



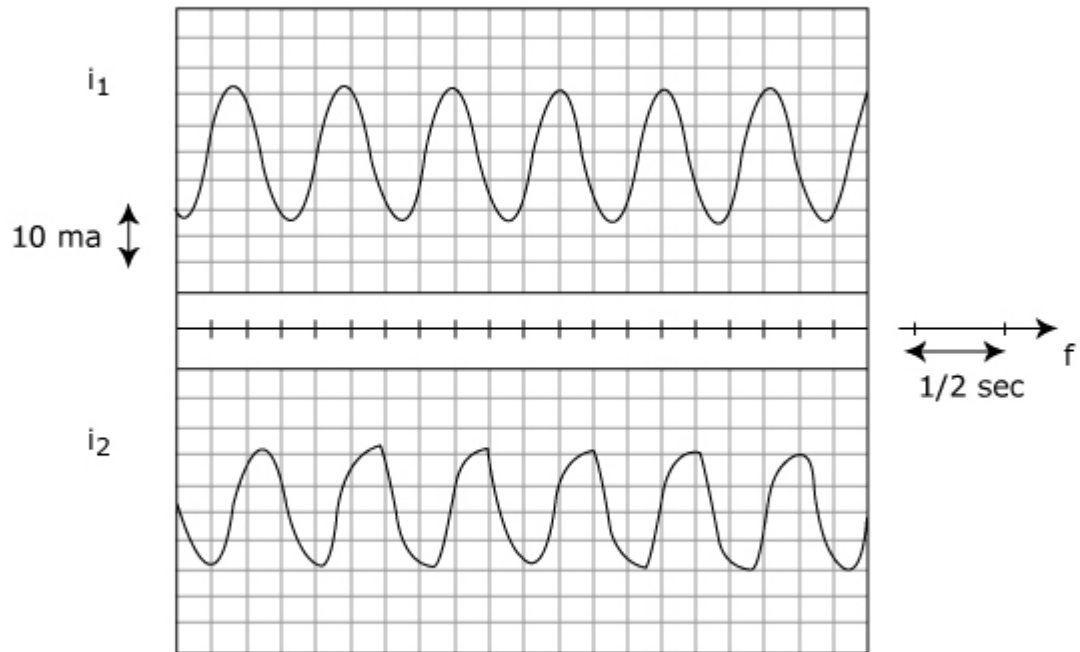
(b)



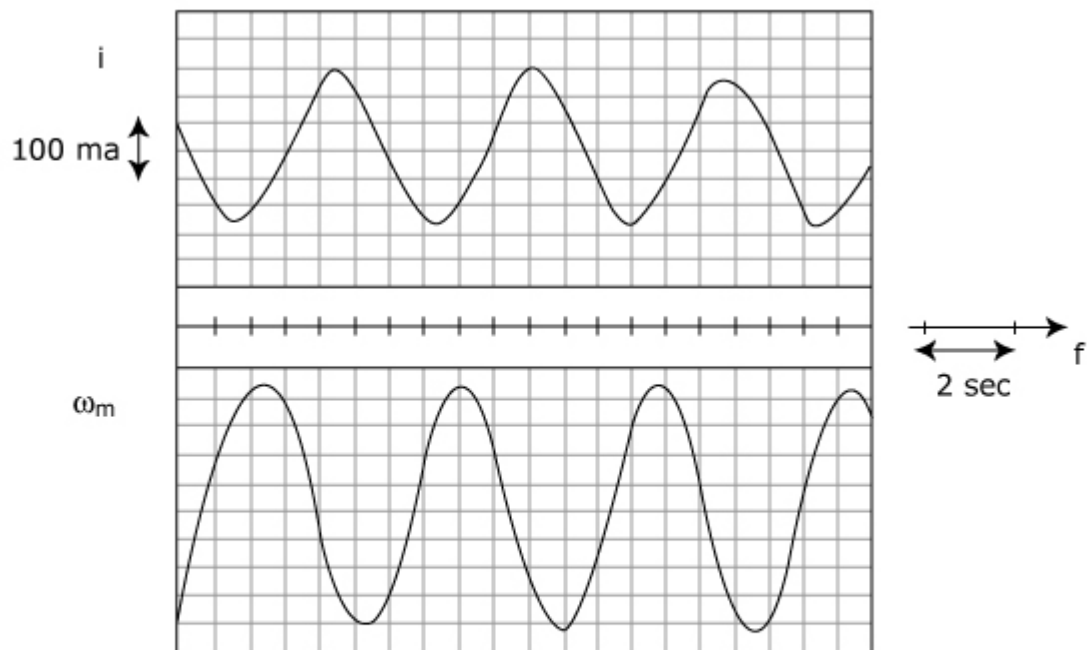
Configuration for obtaining a.c. power from two identical generators. (a) Wiring configuration. (b) Equivalent circuit description.



(a)



(b)



(a) Two-phase currents obtained from a pair of coupled d.c. machines rotating at a speed of 1790 rev/min. (b) Alternating current and speed for the coupled motor-generator combination with $I_f = 0.15\text{ A}$ and generator shaft of 1620 rev/min.